

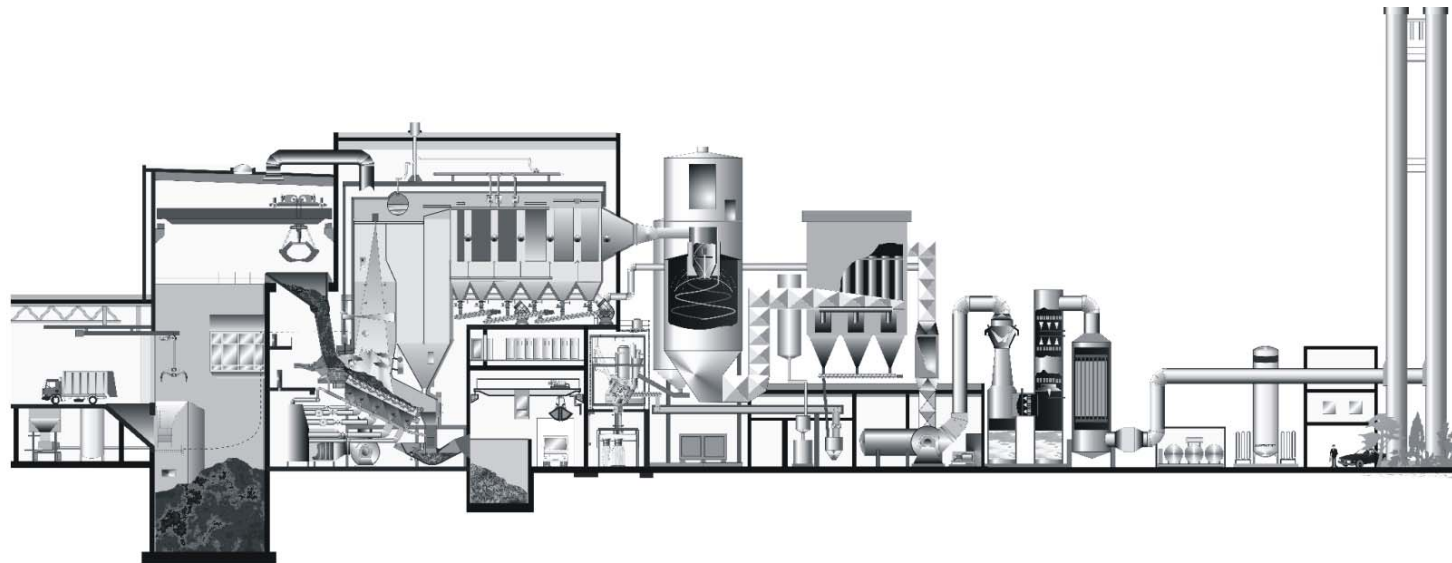
Determination of the energy efficiency by balancing of the WtE-plant

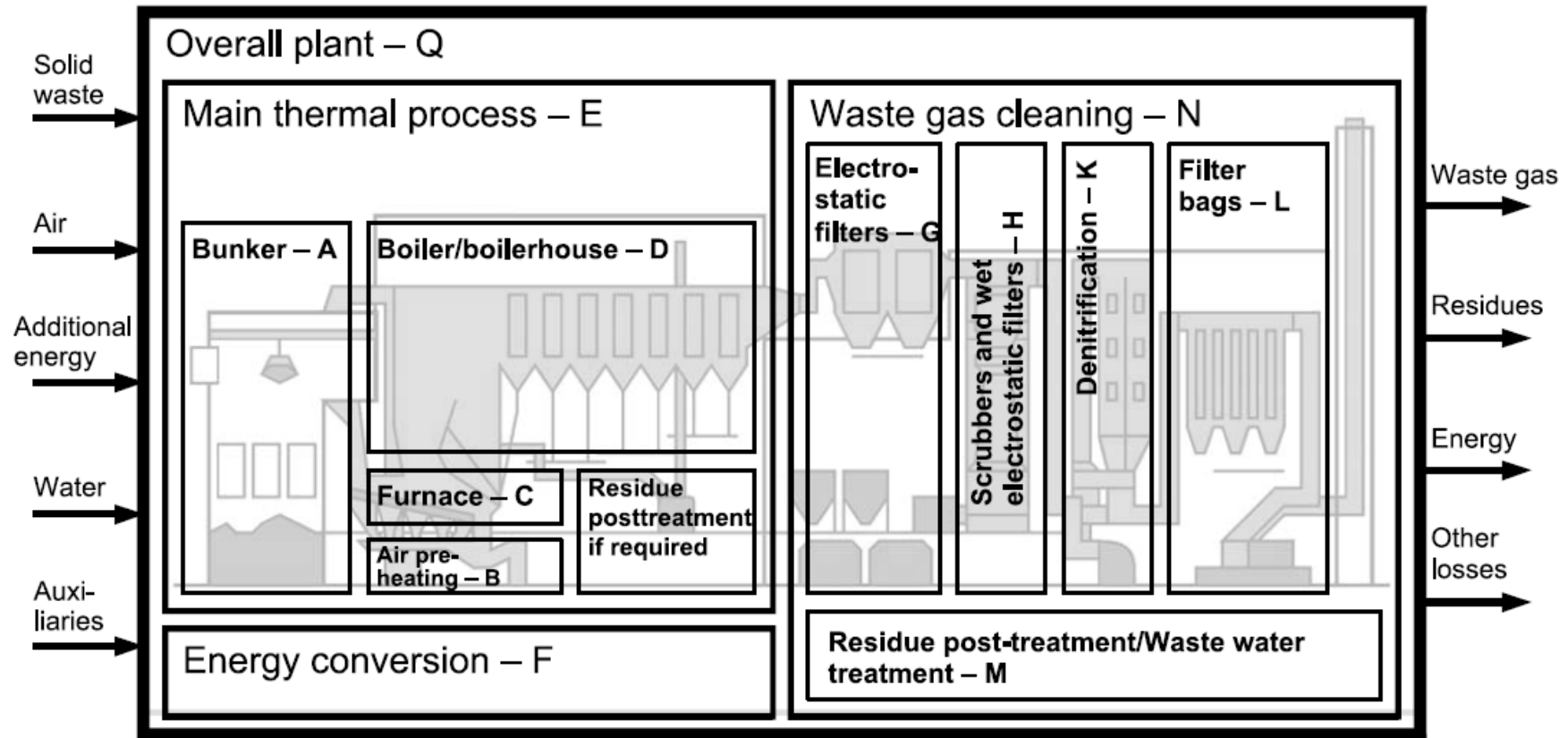
Michael Beckmann

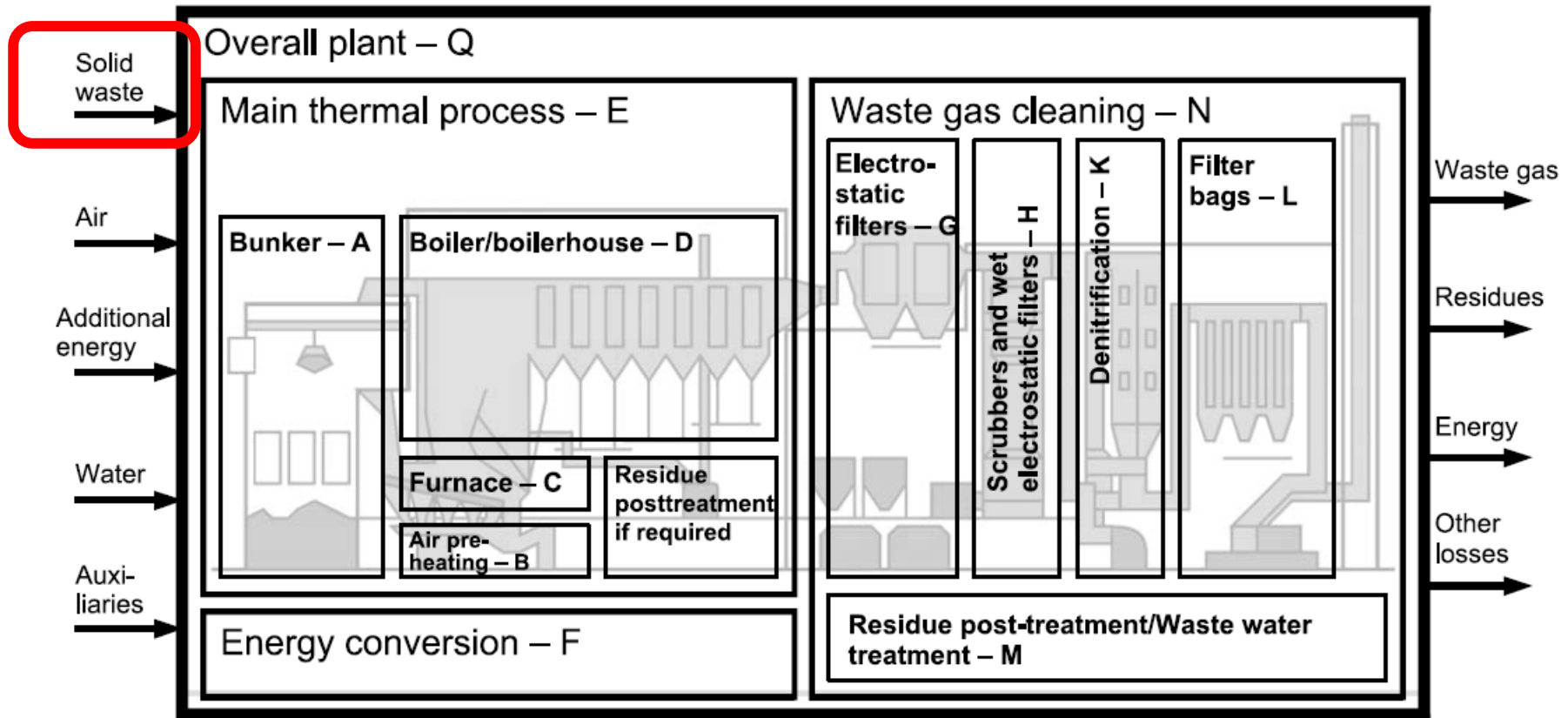
10. March 2014; Karlsruhe

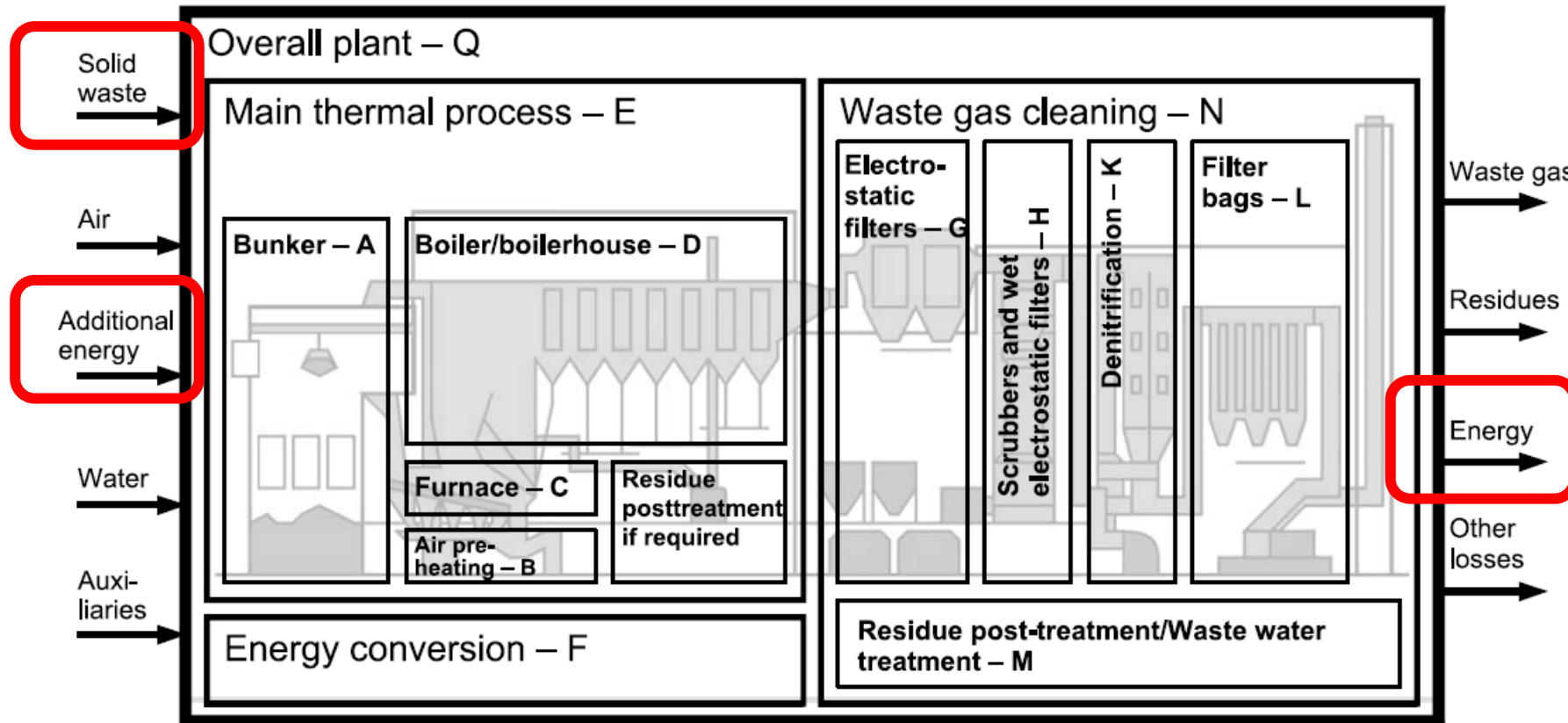


DRESDEN
concept
Exzellenz aus
Wissenschaft
und Kultur

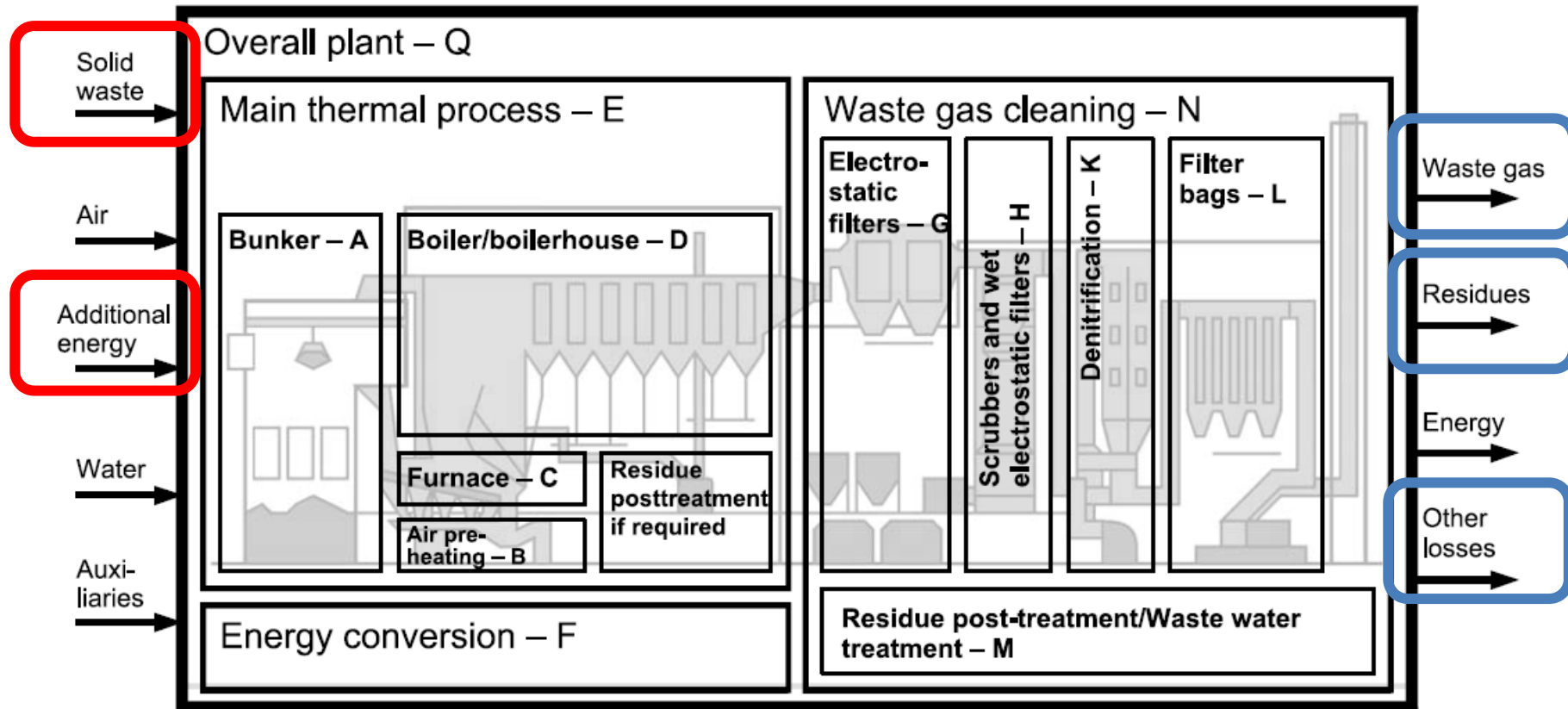




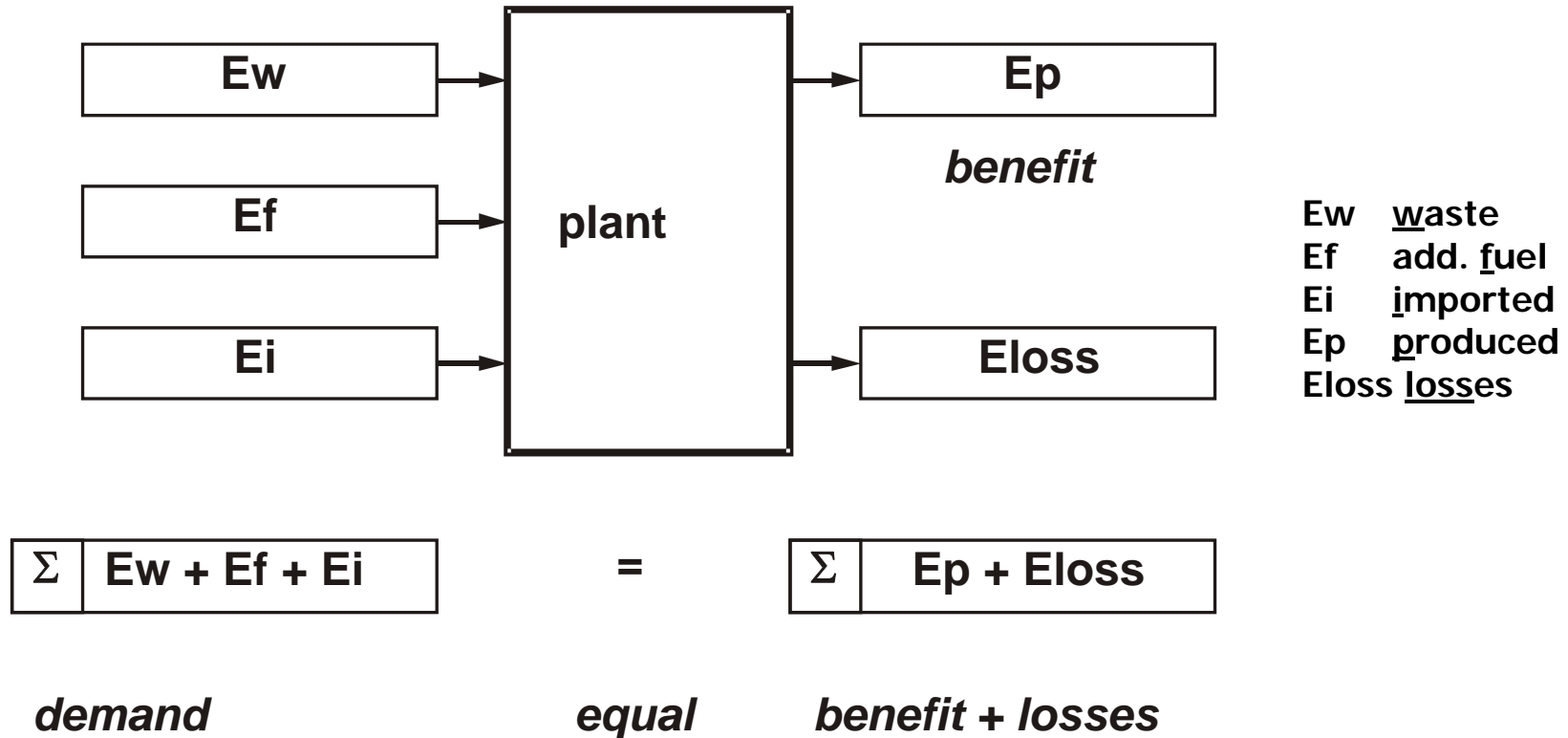




$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{\textit{energy}}{\textit{waste and additional energy}}$$



$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{\textit{demand} - \textit{losses}}{\textit{demand}} = 1 - \frac{\textit{losses}}{\textit{demand}}$$



Ew waste
 Ef add. fuel
 Ei imported
 Ep produced
 Eloss losses

balancing circle 1 \Rightarrow **plant efficiency**

$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p}{E_w + (E_f + E_i)}$$

balancing circle 1 \Rightarrow plant efficiency

$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p}{E_w + (E_f + E_i)}$$

R1

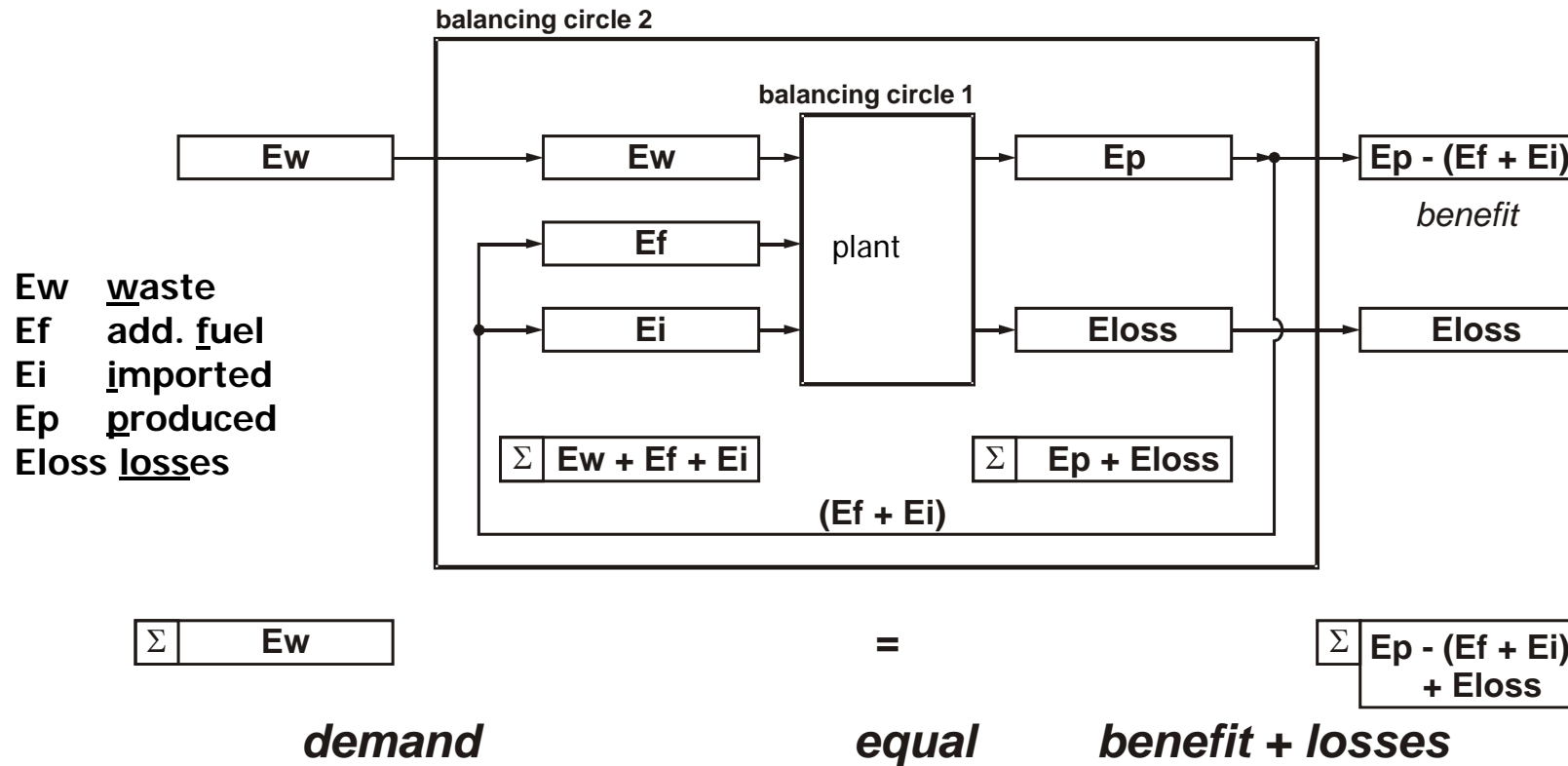
$$R1 = \frac{E_p - (E_f + E_i)}{0,97 * (E_w + E_f)}$$

balancing circle 1 \Rightarrow plant efficiency

$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p}{E_w + (E_f + E_i)}$$

R1

$$R1 = \frac{E_p - (E_f + E_i)}{0,97 * (E_w + E_f)}$$



balancing circle 2 \Rightarrow **net efficiency**

$$\eta_{net} = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p - (E_f + E_i)}{E_w}$$

balancing circle 2 \Rightarrow net efficiency

$$\eta_{net} = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p - (E_f + E_i)}{E_w}$$

R1

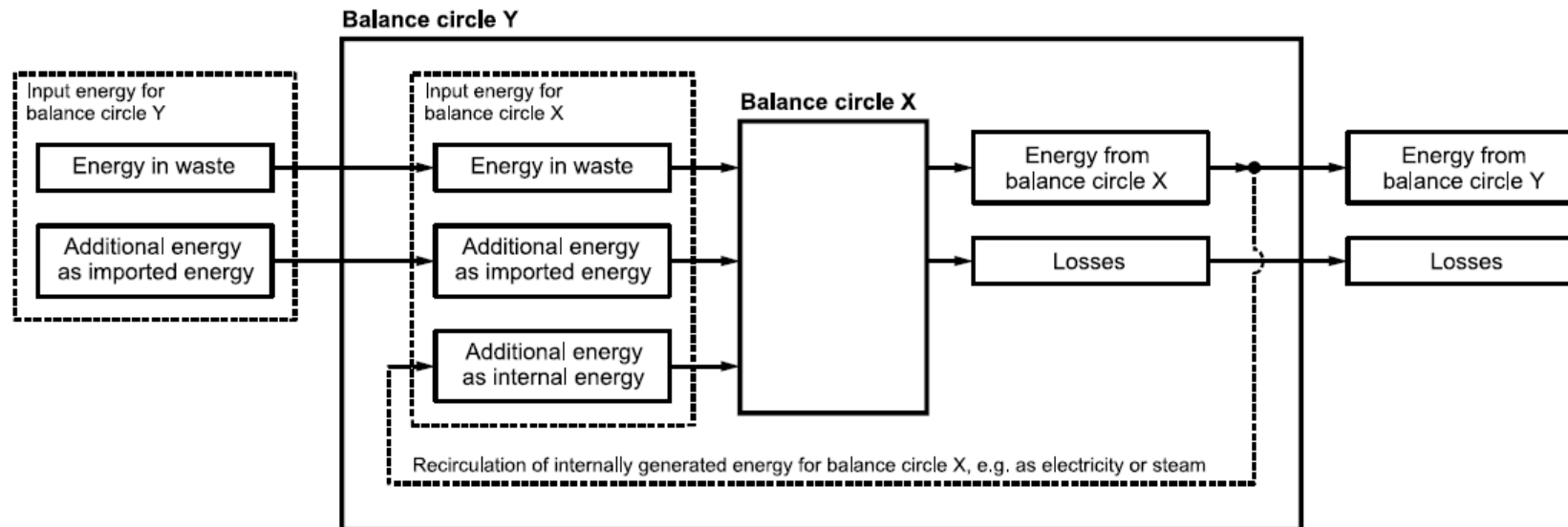
$$R1 = \frac{E_p - (E_f + E_i)}{0,97 * (E_w + E_f)}$$

balancing circle 2 \Rightarrow net efficiency

$$\eta_{net} = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{E_p - (E_f + E_i)}{E_w}$$

R1

$$R1 = \frac{E_p - (E_f + E_i)}{0,97 * (E_w + E_f)}$$



According to VDI 3460 (2)

Classification of Waste-to-energy Plants in Terms of Energy Recovery

VGB PowerTech 10/2007 P 76 – 81.

Authors

Prof. Dr.-Ing. Michael Beckmann
Bauhaus-Universität Weimar
Weimar/Germany.

Ferdinand Kleppmann
President Confederation of
European Waste-to-Energy Plants (CEWEP)
Brussels/Belgium.

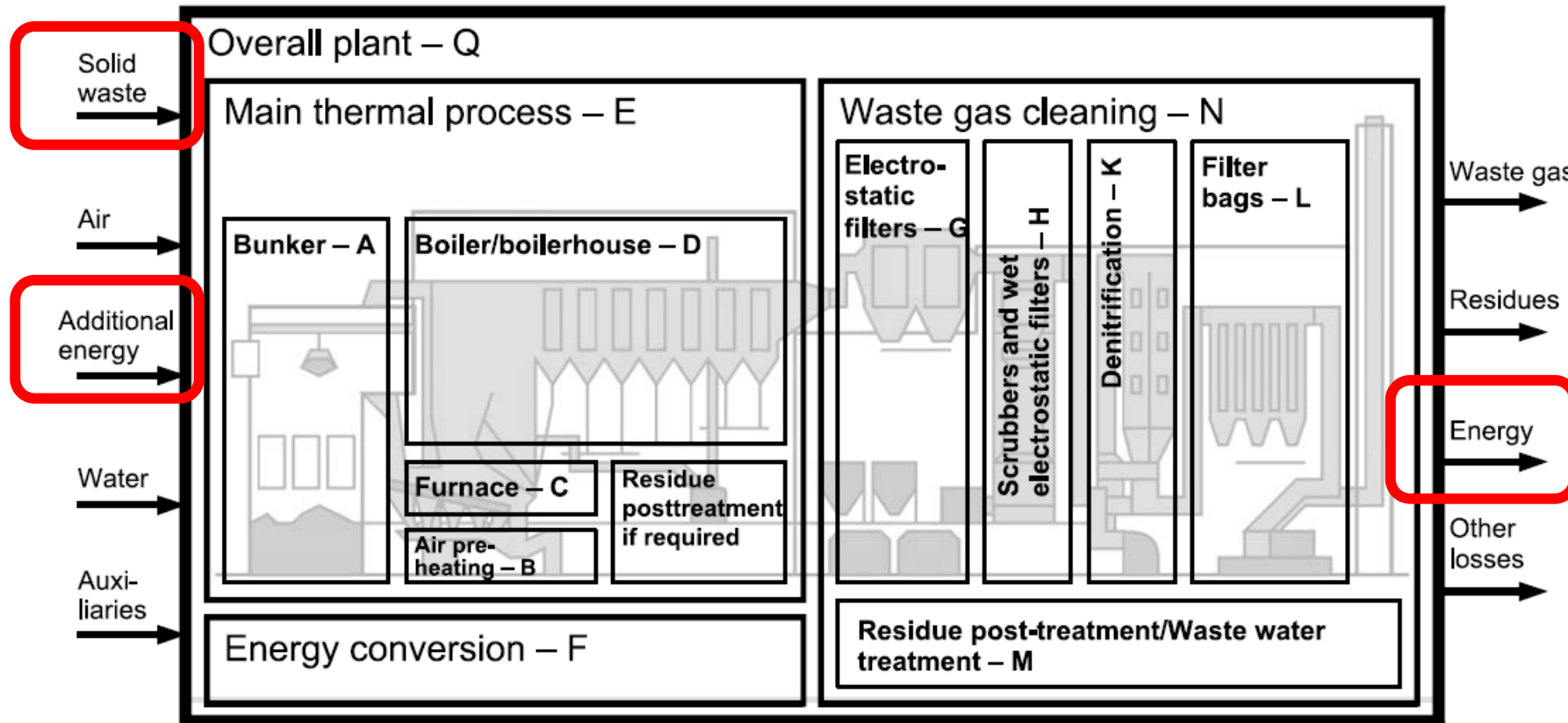
Johannes J.E. Martin
Managing Director
Martin GmbH für Umwelt- und
Energietechnik, München/Germany.

Prof. Dr.-Ing. Reinhard Scholz
Technische Universität Clausthal
Clausthal-Zellerfeld/Germany.

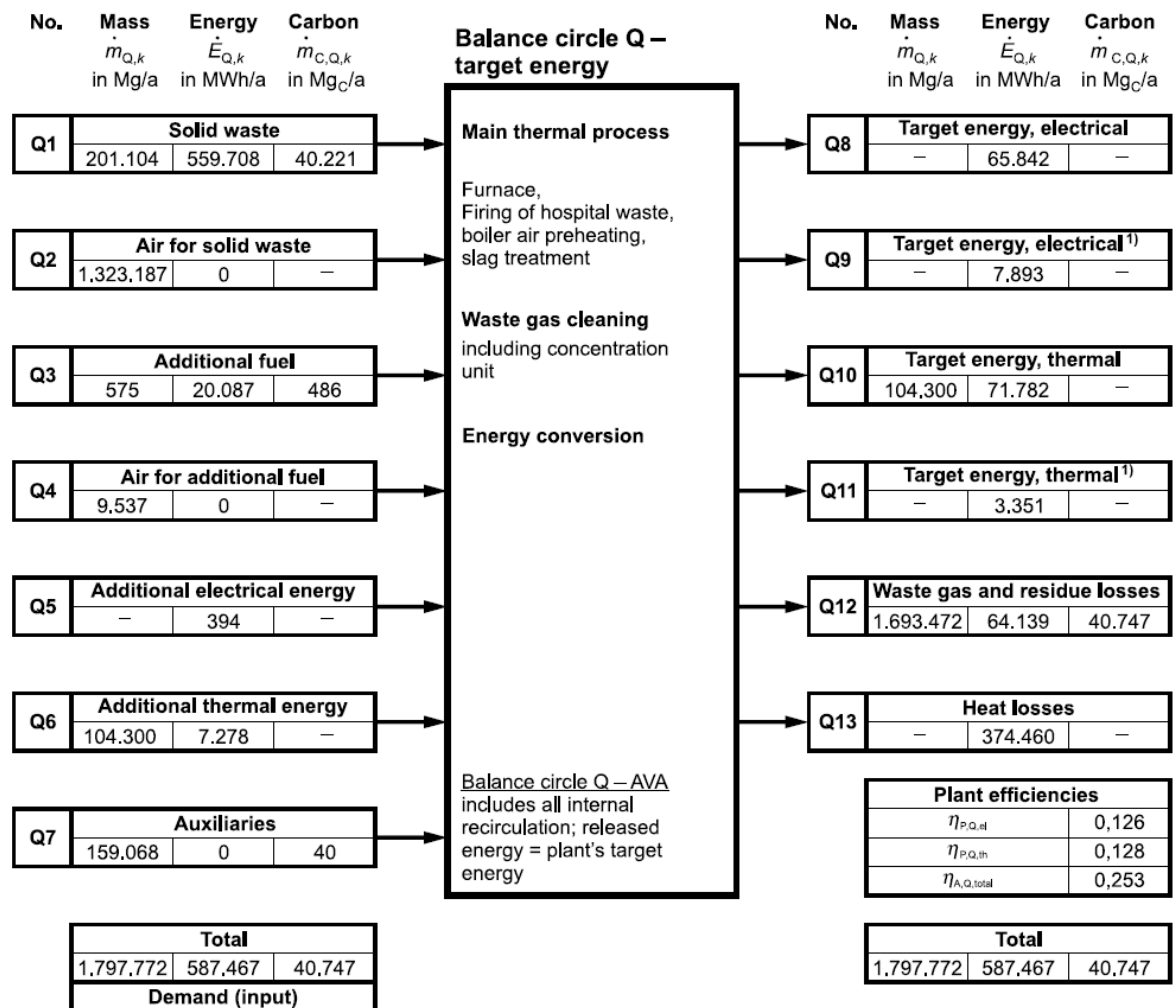
Prof. Dr.-Ing. Helmut Seifert,
Forschungszentrum Karlsruhe GmbH
Karlsruhe/Germany.

Resumé

1. The VDI guideline 3460 [2] is based on known and proven engineering knowledge and forms the basis for assessing the energy efficiency of waste-to-energy plants with particular reference to optimisation.
2. The R1 formula [3] has a politically regulatory function for differentiating between R1 and D10 (R1 as the technical term).
3. When differentiating between the two approaches mentioned above, 1 and 2, it is unnecessary to refer to R1 in VDI guideline 3460.

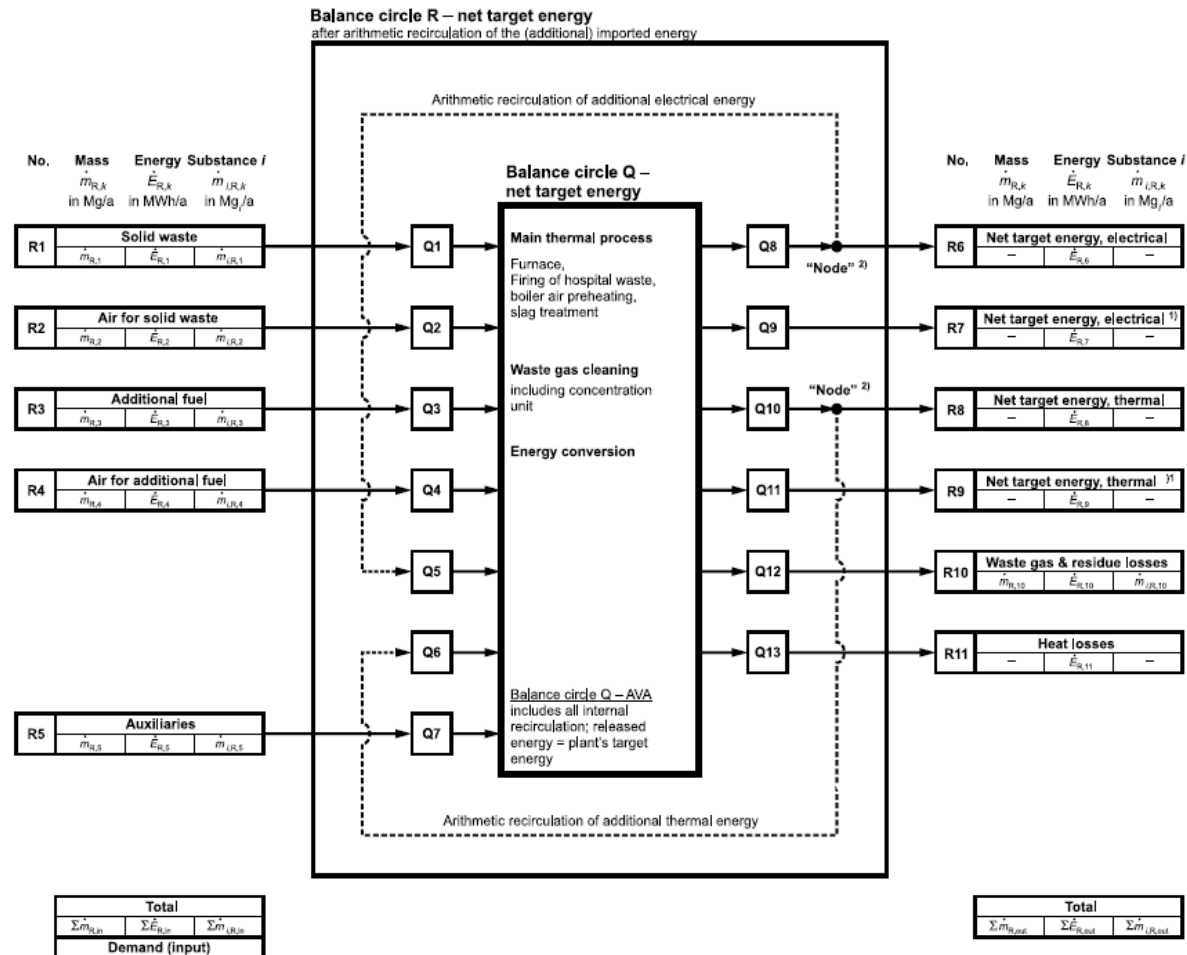


$$\eta_P = \frac{\textit{benefit(output)}}{\textit{demand(input)}} = \frac{\textit{energy}}{\textit{waste and additional energy}}$$



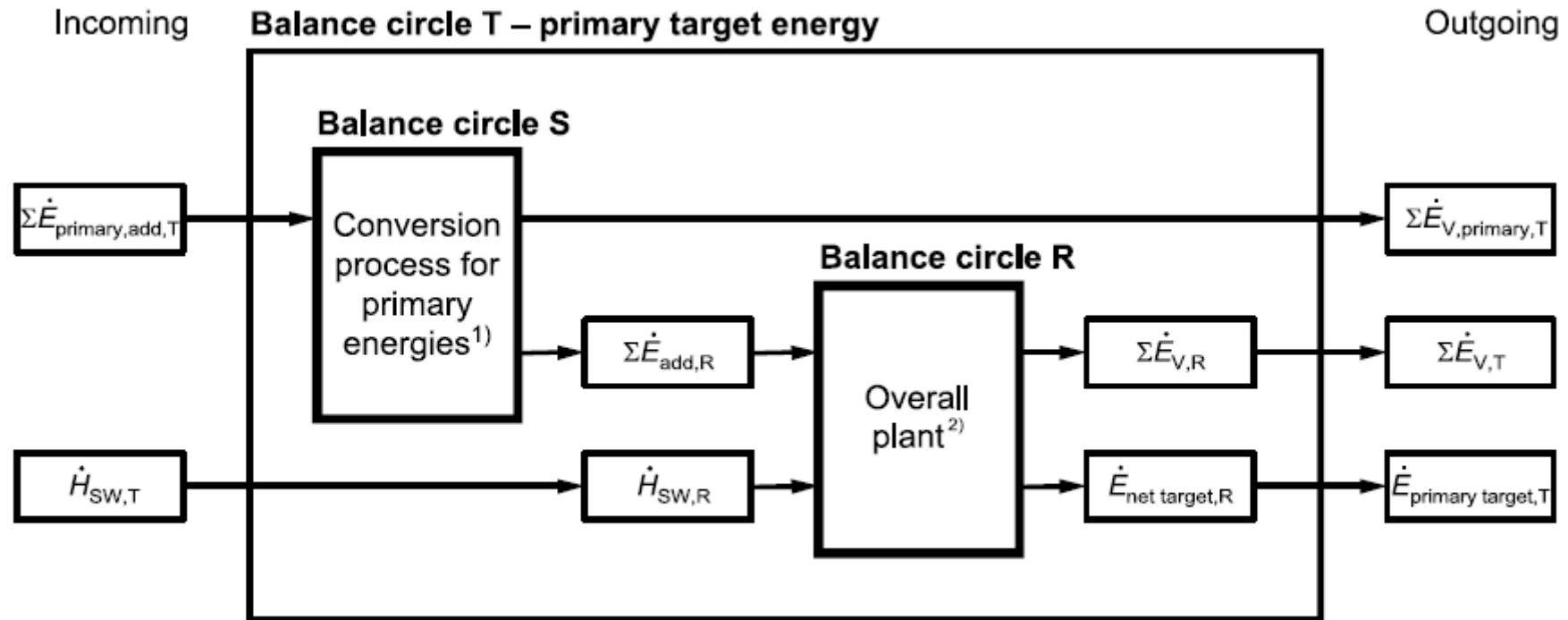
¹⁾ Target energy broken down here in accordance with operator's information into target energy supplied to public services company (Q8 and Q10) and target energy to neighbouring customers on site (for composting, sorting, etc., Q9 and Q11)

According to VDI 3460 (2)



¹⁾ Target energy broken down here in accordance with operator's information into target energy supplied to public services company (Q8 and Q10) and target energy to neighbouring customers on site (for composting, sorting, etc., Q9 and Q11)

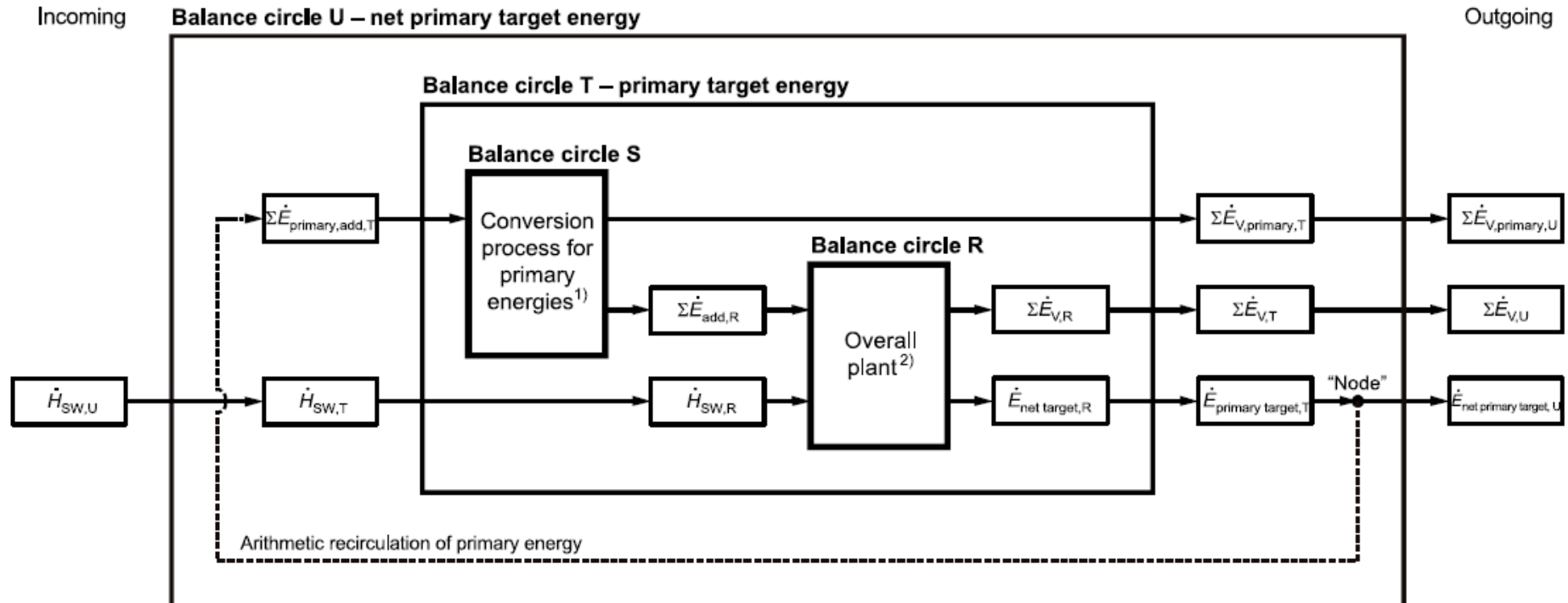
²⁾ Public services company, district heat transfer station, etc.



¹⁾ e.g. generation of electricity, oxygen, etc.

²⁾ including recirculation of thermal and electrical energy

$$\left(\eta_{\text{primary}} = \frac{\dot{E}_{\text{primary target}}}{\dot{H}_{\text{SW}} + \sum \dot{E}_{\text{primary add}}} \right)_T$$

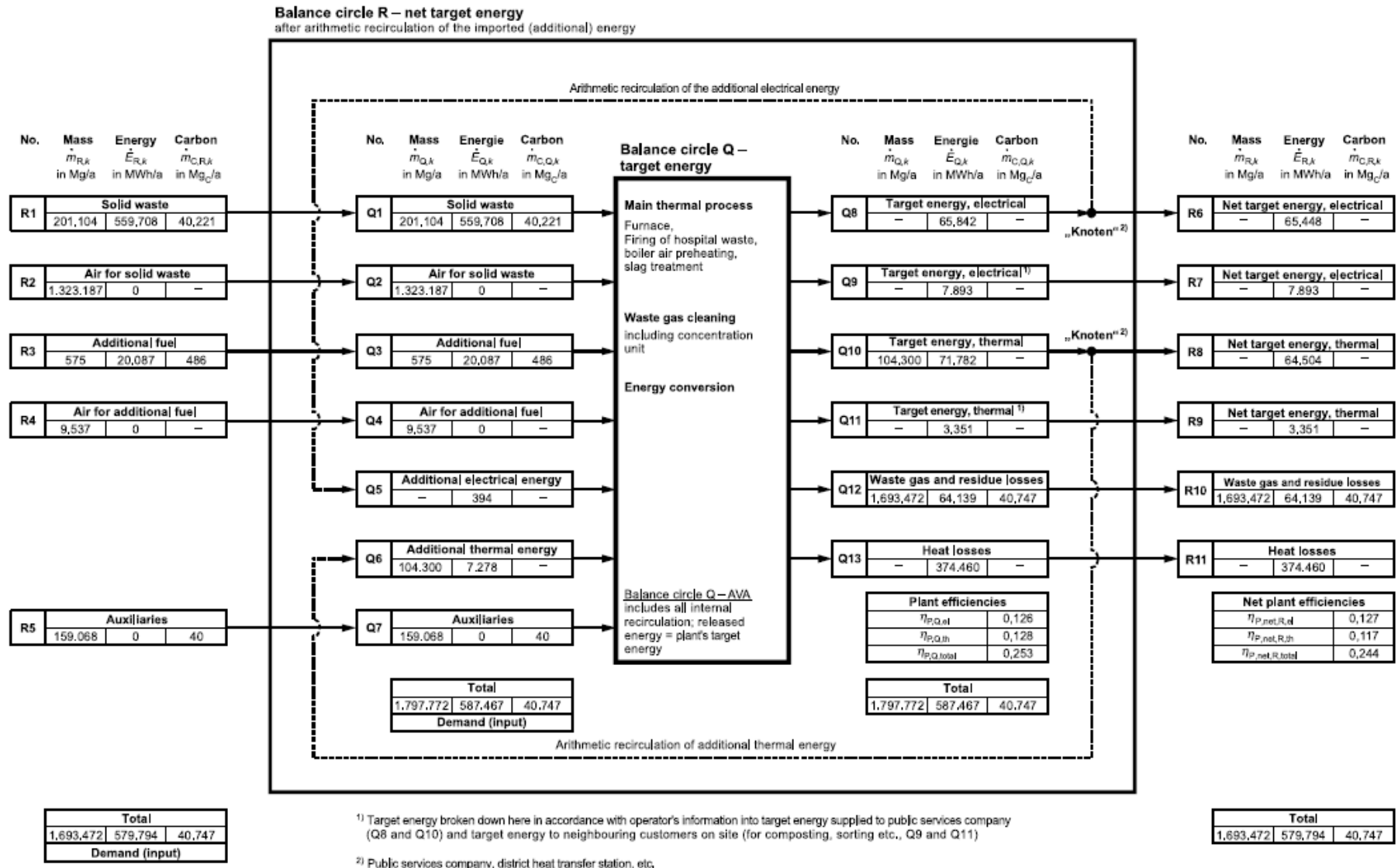


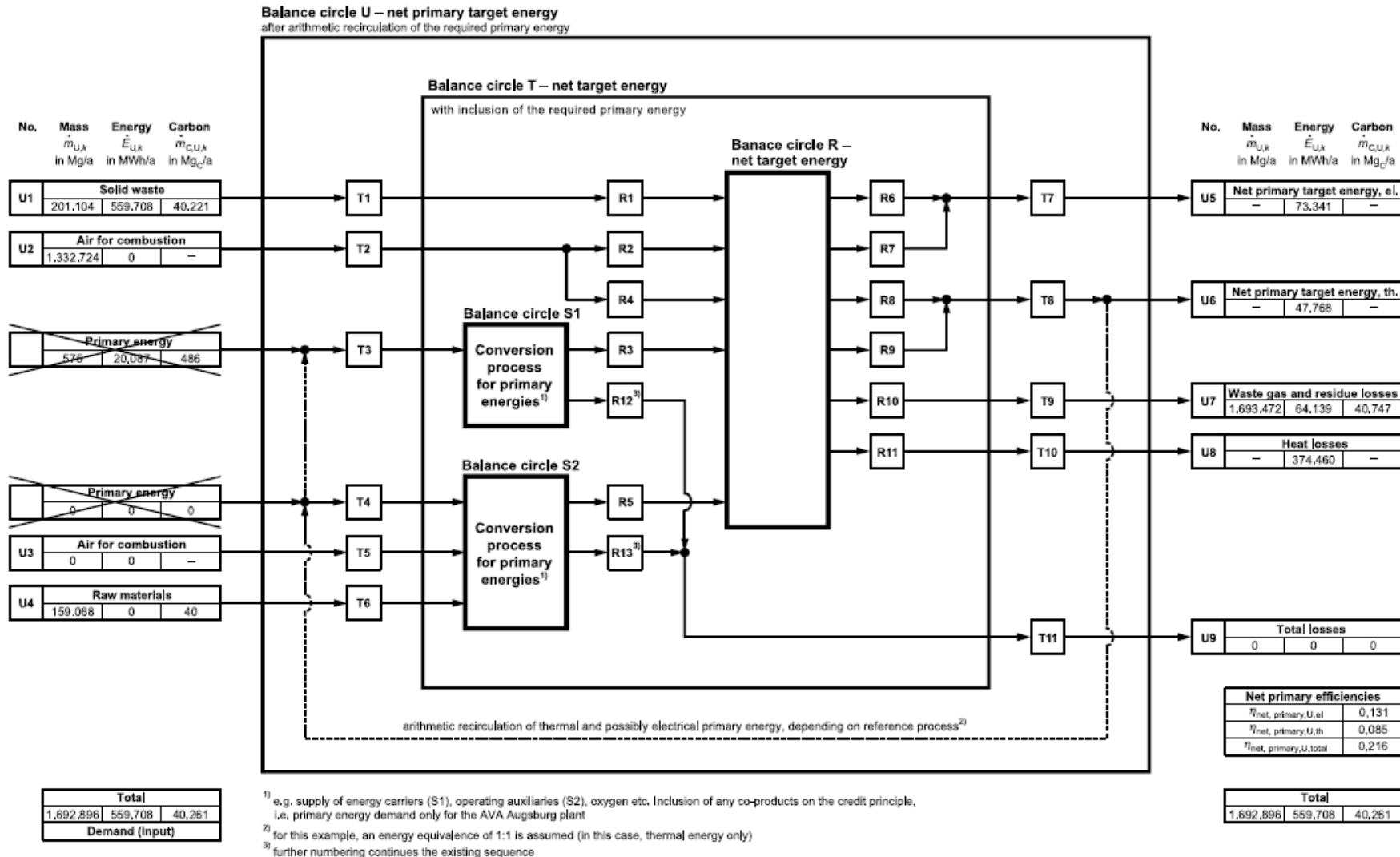
¹⁾ e.g. generation of electricity, oxygen, etc.
²⁾ including recirculation of thermal and electrical energy

$$\left(\eta_{\text{net primary}} = \frac{\dot{E}_{\text{net primary target}}}{\dot{H}_{\text{SW}}} \right)_U$$

$$(\dot{E}_{\text{net primary target}})_U = (\dot{E}_{\text{primary target}} - \sum \dot{E}_{\text{primary,add}})_T$$

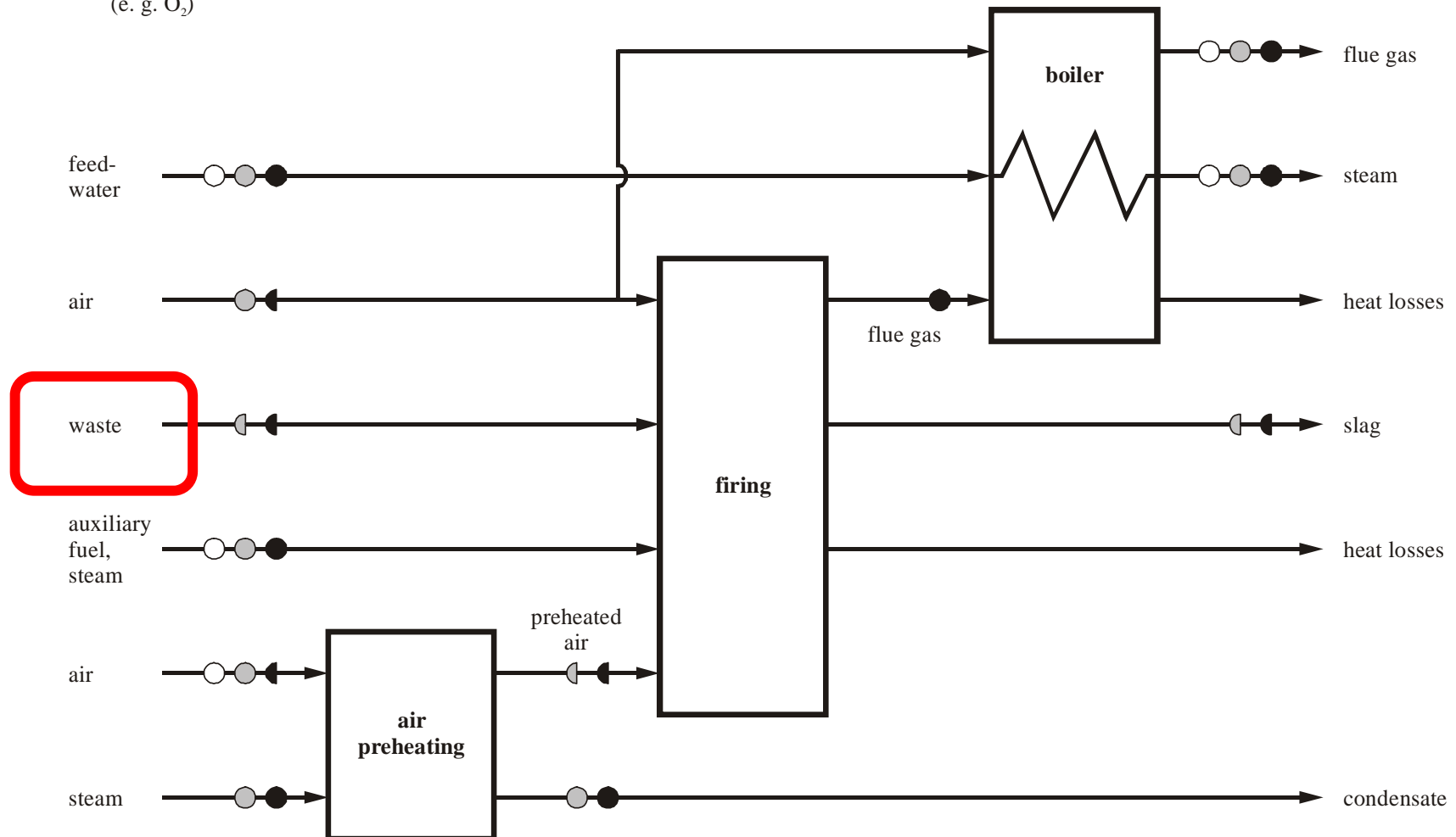
$$\text{for } (\dot{E}_{\text{net primary target}})_U > 0$$

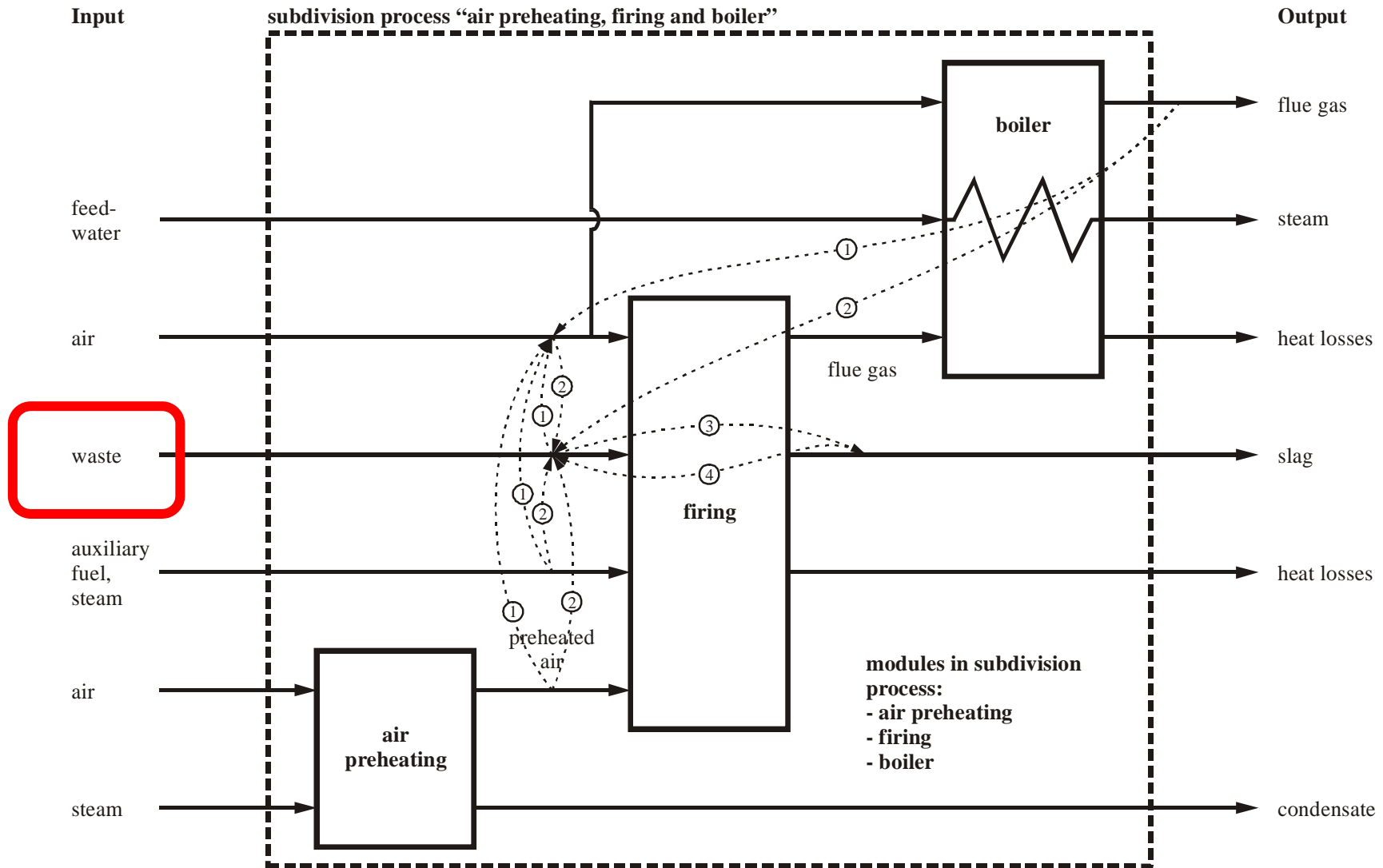


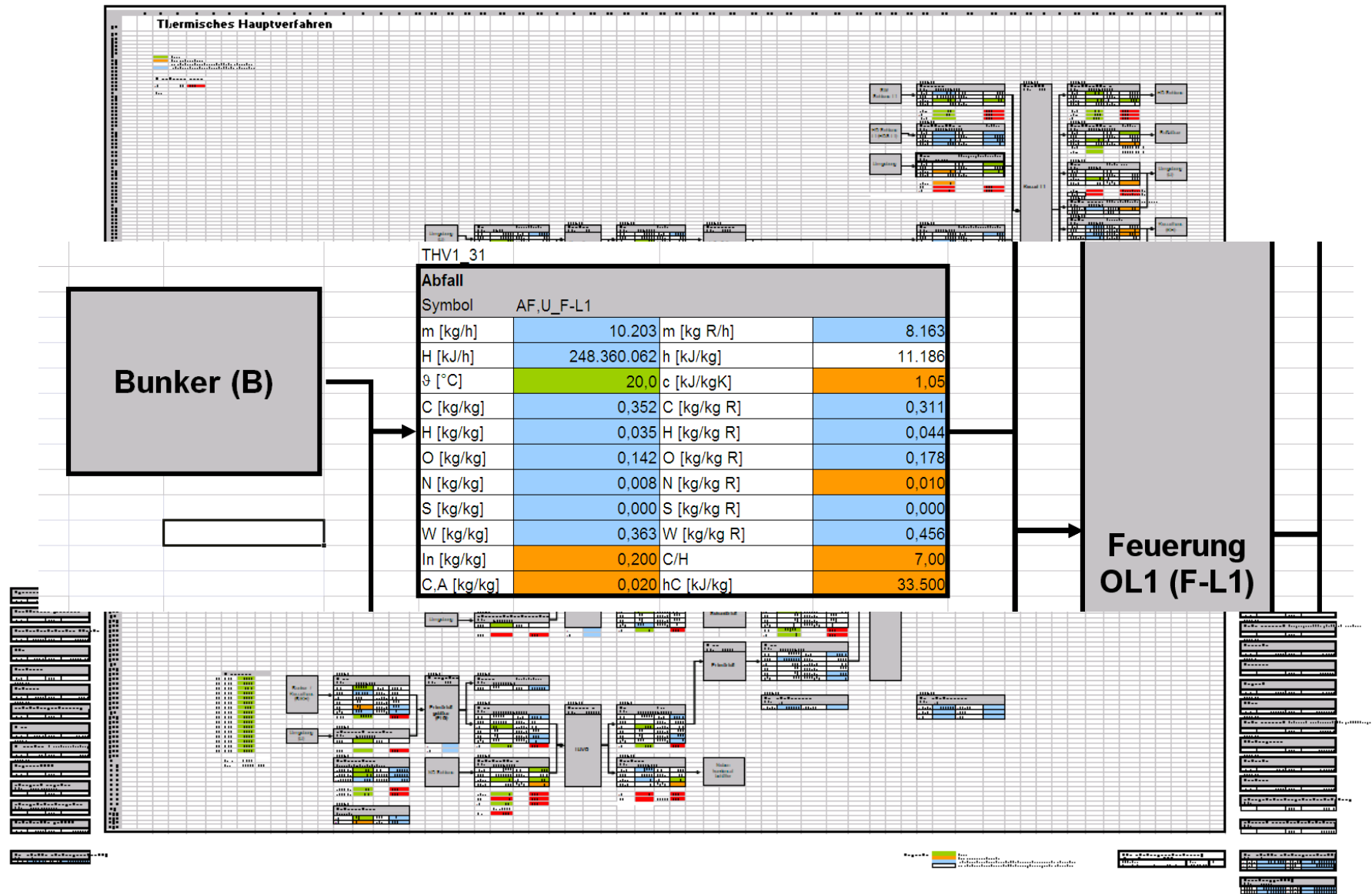


available measuring data and parameters:

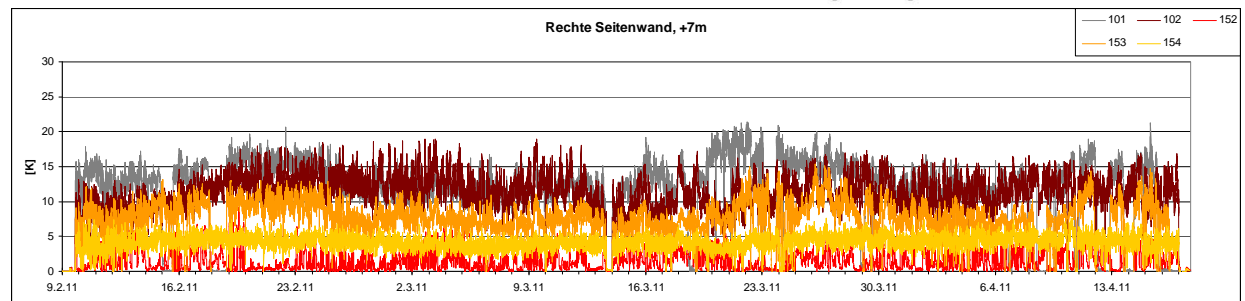
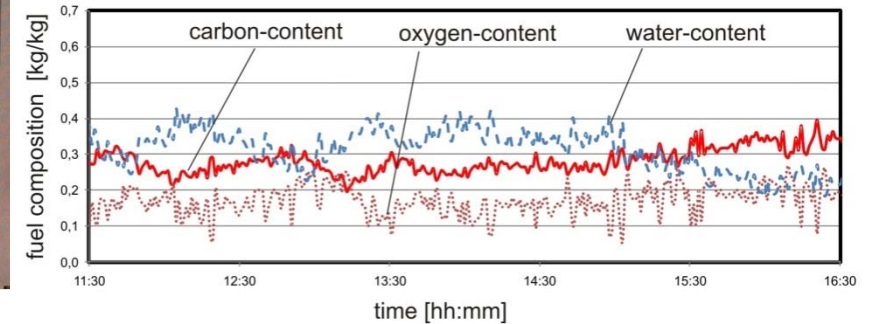
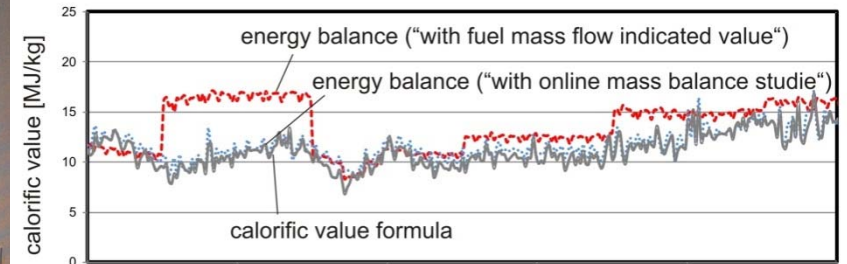
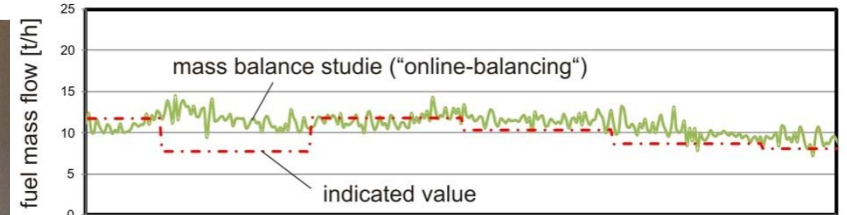
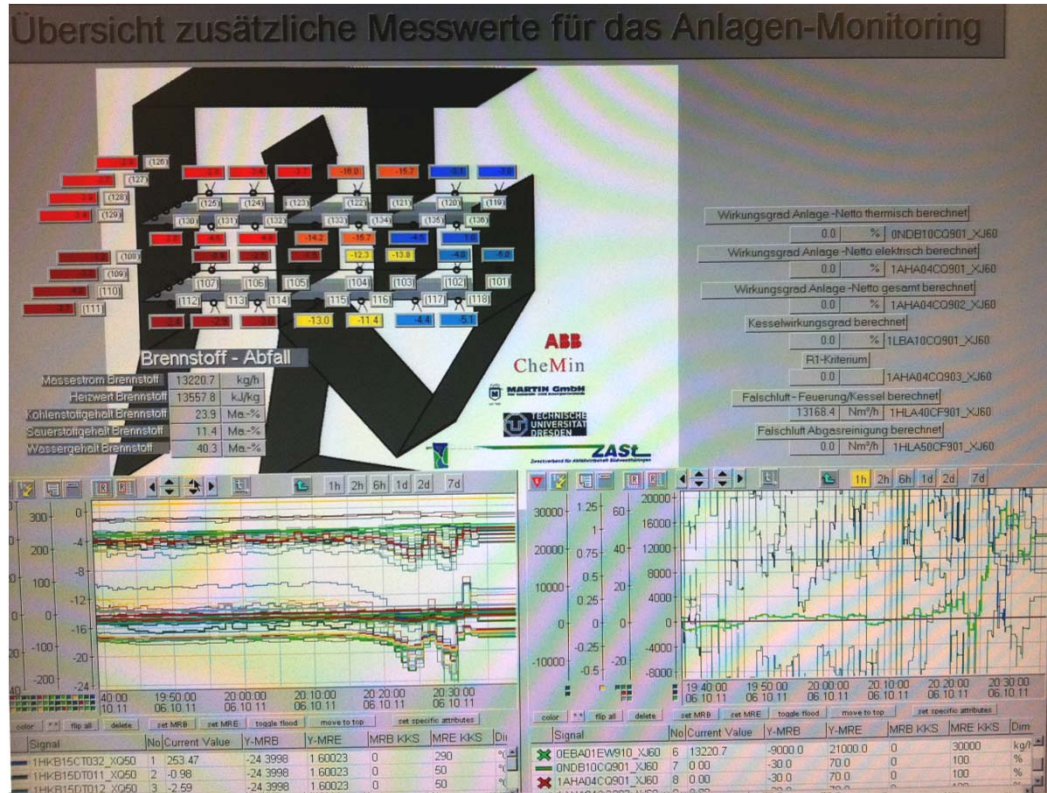
- mass or volume flows
- temperature resp. specific enthalpy (feed water, steam)
- composition
- ◐ composition partial known (e. g. O₂)
- ◑ temperature resp. specific enthalpy assumed







- **285 measuring values for balancing**
- **Reading/recording the measured data signals via the OPC-Server connection**
- **Converting the measured signal corresponding to the calibration of measuring device if necessary**
- **Checking the measured value if the value is within an individually defined ratio (upper and lower limit) and**
- **Checking the measured value - if the value is defined as indicator parameter - to see if it can be allocated to a practically stationary state**



We would like to thank the operators and manufactures of MSWI plants who have supported us
in the development and testing of the *online balancing methode*.



»Wissen schafft Brücken.«